

Power Generation

The present invention relates to power generation  
5 using a lifting body in a fluid flow.

Power is generally obtained from wind using windmills  
which are large relatively expensive structures. Power is  
obtained from water using hydro-electric dams. It would be  
desirable to have alternative, less expensive mechanisms  
10 for obtaining power from fluid flow.

US 6254034 describes a system for electricity  
generation in which wind blows a tethered tractor kite  
downwind. The kite has a single tether wound around a  
windlass drum, which is connected to an electrical  
15 generator and a motor. The cycle for generation of  
electrical power involves a downwind travelling phase and  
an upwind travelling phase. In the downwind phase, the  
downwind travelling kite generates power. It pulls its  
tether off the windlass drum and drives the electrical  
20 generator. In the upwind travelling phase the kite is  
controlled to change its shape or pitch by special  
mechanisms in the kite itself and the motor revolves the  
drum to reel in the tether. This system has several  
25 drawbacks. It requires an electric motor for winding the  
kite in and a special kite tethered by a single tether that  
can be controlled to change its shape or pitch. It is  
unsuitable for generating power from water flow.

According to one aspect of the present invention there  
is provided a power generator comprising: a lifting body  
30 for suspension in a moving fluid; a control station; and  
at least two tethers for tethering the lifting body to the  
control station, wherein the control station is arranged to  
transform oscillating tension in the tethers produced by an  
oscillating movement of the lifting body into mechanical  
35 motion.

According to another aspect of the present invention

there is provided a control station for a power generator using a lifting body in a fluid stream comprising: at least two tied points for the connection of at least two tethers for tethering the lifting body to the control station; and 5 means for transforming oscillating tension in the tethers produced by an oscillating movement of the lifting body into mechanical motion.

According to one aspect of the present invention there is provided a method of extracting power from a fluid flow 10 comprising the steps of: suspending a lifting body in the fluid flow using at least two tethers and transforming an oscillating tension in the tethers produced by an oscillating movement of the lifting body into mechanical motion.

15 Embodiments of the invention provide significant advantages. The lifting body is of very simple construction and does not need any special mechanisms to control its pitch or shape. All the mechanisms for controlling the pitch of the lifting body and generating power are located 20 in the control station which can be located in an easily accessible position. The control station may be small and easily portable. It can be of a simple and robust construction. The power generator is particularly useful in the Third World.

25 For a better understanding of the present invention and to understand how the same may be brought into effect, reference will now be made by way of example only to the following drawings in which:

Figure 1 illustrates a power generator according to 30 one embodiment of the present invention;

Figures 2a, 2b, 2c and 2d illustrate the cyclic rotation of the flywheel used for power generation;

Figures 3a, 3b, 3c and 3d illustrate the oscillation and reciprocation of the connecting rod head attached to 35 the flywheel;

Figures 4a, 4b, 4c and 4d illustrate the oscillation

of the lifting body tethered to the oscillating connecting rod head;

Figure 5a illustrates the variation of the pitch angle (alpha) of the lifting body with the angle of rotation 5 (Beta) of the flywheel;

Figure 5b illustrates the variation of the tension in the tethers of the lifting body with the angle of rotation (Beta) of the flywheel; and

Figure 5c illustrates the variation of the 10 instantaneous work done with the angle of rotation (Beta) of the flywheel.

Figure 1 illustrates a power generator 2 comprising a lifting body 4, a control station 30 and first and second tethers 6 & 8 connecting the lifting body to the control 15 station.

The lifting body is in a fluid flow F and the control station 30 is resting on an easily accessible surface 32, such as the ground, the deck of a boat or the top of a building. The control station 30 remains stationary on the 20 surface 32 and the fluid flow F lifts and drags the lifting body 4. The first tether 6 and the second tether 8 are of fixed length and, in use, are under tension caused by the lift and drag of the lifting body 4. The points at which the first tether 6 and the second tether 8 connect to the 25 lifting body 4 lie in a substantially straight line connecting the leading and trailing edges of the lifting body 4. The tethers 6, 8 are used to alter the angle of incidence (or pitch) of the lifting body 4 and hence the lift and drag.

30 The control station 2 controls pitch of the lifting body 4 and extracts power from the oscillatory modulation in the tension in the tethers 6, 8 caused by the variation in lift and drag. The control station 30 comprises a flywheel 26 mounted for rotation in a counter clockwise 35 direction which stores the generated power. A 'T' shaped connecting rod 16 is connected at one end to the side of

the flywheel at a distance from the flywheel's axis of rotation by a crank pin 28. The 'T' shaped connecting rod 16 has a connecting rod head 14 at its other end. The connecting rod head 14 has a first tie point 10 and a second tie point 12. In use, the first tether 6 is connected to the first tie point 10 and the second tether 8 is connected to the second tie point 12. The connecting rod head 14 is constrained to move along a line of constraint 22, by the constraining link 20 which is connected at one end to a fixed pivot point 18 and at the other end to the connecting rod via a pivoting connection 24. The line of constraint 22 will be curvilinear but will approximate to a rectilinear line for embodiments in which the constraining link 20 is long. For ease of illustration, the line of constraint in Figure 1, has been shown as a rectilinear line. Other mechanisms can be used to control the rocking and translational movements which respectively provide control and power extraction.

The operation of the power generator 2 can be understood by referring to Figs 2a to 4d. Figures 2a, 2b, 2c and 2d illustrate the cyclic rotation of the flywheel 26. The position of the flywheel 26 within a rotation is denoted using the angle of rotation Beta which is 270 degrees, 0 degrees, 90 degrees and 180 degrees respectively in Figures 2a, 2b, 2c and 2d. Figures 3a, 3b, 3c and 3d illustrate the oscillation and reciprocation of the connecting rod head 14 attached at the crank pin 28 to the flywheel 26 by the connecting rod 16. The oscillation/rocking of the connecting rod head 14 provides control of the pull generated by the lifting body and the reciprocating/translational movement of the connecting rod 16 provides for power extraction. When Beta is 270 degrees, the connecting rod head 14, as shown in Fig 3a, is at its maximum displacement away from the flywheel 26 and is tilted at an intermediate angle so that the first tie point 10 leads the second tie point 12. When Beta is

0/360 degrees, the connecting rod head 14, as shown in Fig 3b, is at an intermediate displacement away from the flywheel 26 and is tilted at a minimum angle. In this particular embodiment, the minimum angle is zero so that 5 the first tie point 10 is level with the second tie point 12. When Beta is 90 degrees, the connecting rod head 14, as shown in Fig 3c, is at a minimum displacement away from the flywheel 26 and is tilted at an intermediate angle so that the first tie point 10 leads the second tie point 12. When 10 Beta is 180 degrees, the connecting rod head 14, as shown in Fig 3d, is at an intermediate displacement away from the flywheel 26 and is tilted at a maximum angle so that the first tie point 10 leads the second tie point 12.

As the connecting rod head 14 moves towards the 15 flywheel (return-stroke), it moves from the position illustrated in Fig 3a through the position illustrated in Fig 3b to the position illustrated in Fig 3c. It moves from being at an intermediate angle to being flat and then returns to the intermediate angle. As the connecting rod 20 head 14 moves away from the flywheel (out-stroke), it moves from the position illustrated in Fig 3c through the position illustrated in Fig 3d to the position illustrated in Fig 3a. It moves from being at an intermediate angle to being at a maximum angle and then returns to the 25 intermediate angle.

Figures 4a, 4b, 4c and 4d illustrate the oscillation of the lifting body 4 tethered to the oscillating connecting rod head 14. The lifting body and the connecting rod head 14 oscillate in phase.

30 When Beta is 270 degrees, the pitch angle (alpha) of the lifting body 4, as shown in Fig 4a, is at an intermediate value. The lift and drag created by the lifting body 4 in the fluid flow F is at an intermediate value, and the tension in the tethers 6,8 is at an 35 intermediate value.

When Beta is 360 degrees, the pitch angle (alpha) of

the lifting body 4, as shown in Fig 4b, is at a minimum (zero) value. The lift and drag created by the lifting body 4 in the fluid flow F is at an minimum value, and the tension in the tethers 6, 8 is at a minimum value.

5 When Beta is 90 degrees, the pitch angle (alpha) of the lifting body 4, as shown in Fig 4c, is at an intermediate value. The lift and drag created by the lifting body 4 in the fluid flow F is at an intermediate value, and the tension in the tethers 6,8 is at an  
10 intermediate value.

When Beta is 180 degrees, the pitch angle (alpha) of the lifting body 4, as shown in Fig 4d, is at a maximum value. The lift and drag created by the lifting body 4 in the fluid flow F is at a maximum value, and the tension in  
15 the tethers 6, 8 is at a maximum value.

As the lifting body moves from the position illustrated in Fig 4a through the position illustrated in Fig 4b to the position illustrated in Fig 4c, the tension in the tethers 6, 8 is modulated. It starts with an  
20 intermediate value then achieves a minimum value and finishes with an intermediate value.

As the lifting body 4 moves from the position illustrated in Fig 4c through the position illustrated in Fig 4d to the position illustrated in Fig 4a, the tension in the tethers 6, 8 is modulated. It starts with an intermediate value, then achieves a maximum value and finishes with at an intermediate value.

The oscillation of the pitch angle (alpha) of the lifting body 4 with the rotation angle (Beta) of the  
30 flywheel is illustrated in Fig 5a and the oscillation of the tension in the tethers 6, 8 of the lifting body 4 with the rotation angle (Beta) of the flywheel 26 is illustrated in Fig 5b. Figure 5c illustrates the variation of the instantaneous work done with the rotation angle (Beta) of  
35 the flywheel.

The references (a) on Figs 5a, 5b and 5c illustrate

the pitch angle (alpha), the tension in the tethers 6, 8 and the instantaneous work done when Beta is 270 degrees. The references (b) on Figs 5a, 5b and 5c illustrate the pitch angle (alpha), the tension in the tethers 6, 8 and the instantaneous work done when Beta is 0 degrees. The references (c) on Figs 5a, 5b and 5c illustrate the pitch angle (alpha), the tension in the tethers 6, 8 and the instantaneous work done when Beta is 90 degrees. The references (d) on Figs 5a, 5b and 5c illustrate the pitch angle (alpha), the tension in the tethers 6, 8 and the instantaneous work done when Beta is 180 degrees.

During the return-stroke (a), (b), (c) work is done by the flywheel. This work is provided by the angular momentum of the flywheel. During the out-stroke (c), (d), (e) work is done on the flywheel. The work done on the flywheel during the out-stroke (illustrated by area A in Fig. 5c) is greater than the work done by the flywheel during the return-stroke (illustrated by area B in Fig. 5c). There is therefore a net energy gain over each rotation of the flywheel, which can be used to drive an electricity generator, pump or other device.

The power generator 2 transforms energy in the fluid flow F into a rotation of the flywheel 26. The rotation of the flywheel 26 can be used to produce electricity, operate a pump or produce reciprocating motion.

In the foregoing, the first tether 6 and the second tether 8 are attached to a single lifting body 4. In other embodiments, multiple lifting bodies 4 can be stacked and each attached to the first tether 6 and the second tether 8.

In the foregoing the control station 30 has a single flywheel 26 and two tethers 6, 8. In other embodiments, the control station 2 may have multiple flywheels 26 connected together using cranks. Each of the multiple flywheels 26 would be attached to at least one lifting body 4 by two tethers 6, 8.

The fluid flow may be erratic, for example in gusting winds. To improve operability in such conditions, embodiments of the invention may have a deformable lifting body 4. Alternatively, a suspension is used. The suspension 5 preferably has a spring or other elastic element between the connecting rod head 14 and each tether 6, 8. A damper may be attached in parallel to the spring.

In other embodiments, a slow response damper may be incorporated in the connecting rod above the pivoting 10 connection 24 to accommodate changes in kite height with wind speed.

In other embodiments, the tethers are deformable to provide adaptation to different wind conditions and/or the 'T' shaped connecting rod 16 is deformable (with 15 appropriate damping) to provide adaptation to different wind conditions.

In other embodiments, the constraining link 20 may be extendible. In Figure 1, the constraining link has a first length so that the connecting rod head 14 is constrained to 20 move along a line of constraint 22 to the left of the axis of the flywheel 26. This allows the power generator 2 to extract power from fluid flow in the direction right to left. According to the current embodiment, the constraining link may be extended to a second length, 25 longer than the first length, so that the line of constraint 22 is positioned to the right of the axis of the flywheel 26 and the power generator 2 is able to extract power from a fluid flow from left to right. This is particularly useful for extracting power from tidal water 30 movements.

In one application of embodiments of the invention, the fluid flow is wind and the lifting body 4 is an aircraft such as a kite or aerofoil. The control station 30 is preferably mounted on bearings so that it can rotate as 35 the wind direction changes. The control station 30 is arranged with the axis of rotation of the flywheel 26

vertical and the tethers in a roughly vertical plane. The aircraft may comprise a lighter than air structure (helium filled) to prevent collapse and maintain altitude when there is no wind and help maintain lift during operation.

5 In another application of embodiments of the invention, the fluid flow is free streaming water which may be found in a river, an estuary, tidal flow or possibly in gross sea movements and the lifting body 4 is an otter board. When the water is provided by a river, the control 10 station 30 is preferably placed on a river bank with the axis of rotation of the flywheel 26 vertical and the tethers in a roughly vertical plane. The otter board remains permanently under the water surface and is given lift by buoyancy in the otter board or by using separate 15 floats.

In another application of embodiments of the invention, the fluid flow is free streaming water which may be found in a river, an estuary, tidal flow or possibly in gross sea movements and the lifting body 4 is an otter 20 board. When the water is provided by a river, the control station 30 is preferably placed on a pontoon or moored raft in the river with the axis of rotation of the flywheel 26 horizontal and the tethers in a roughly horizontal plane. The otter board remains under the water surface for the 25 out-stroke but floats on the surface of the water for at least part of the return-stroke to significantly reduce drag on this part of the cycle.

Whilst endeavouring in the foregoing specification to draw attention to those features of the invention believed 30 to be of particular importance it should be understood that the Applicant claims protection in respect of any patentable feature or combination of features hereinbefore referred to and/or shown in the drawings whether or not particular emphasis has been placed thereon.